

***Actively Cooled Silicon Lightweight Mirrors for Far
Infrared and Submillimeter Optical Systems
Contract No. NNM04AA91C4***



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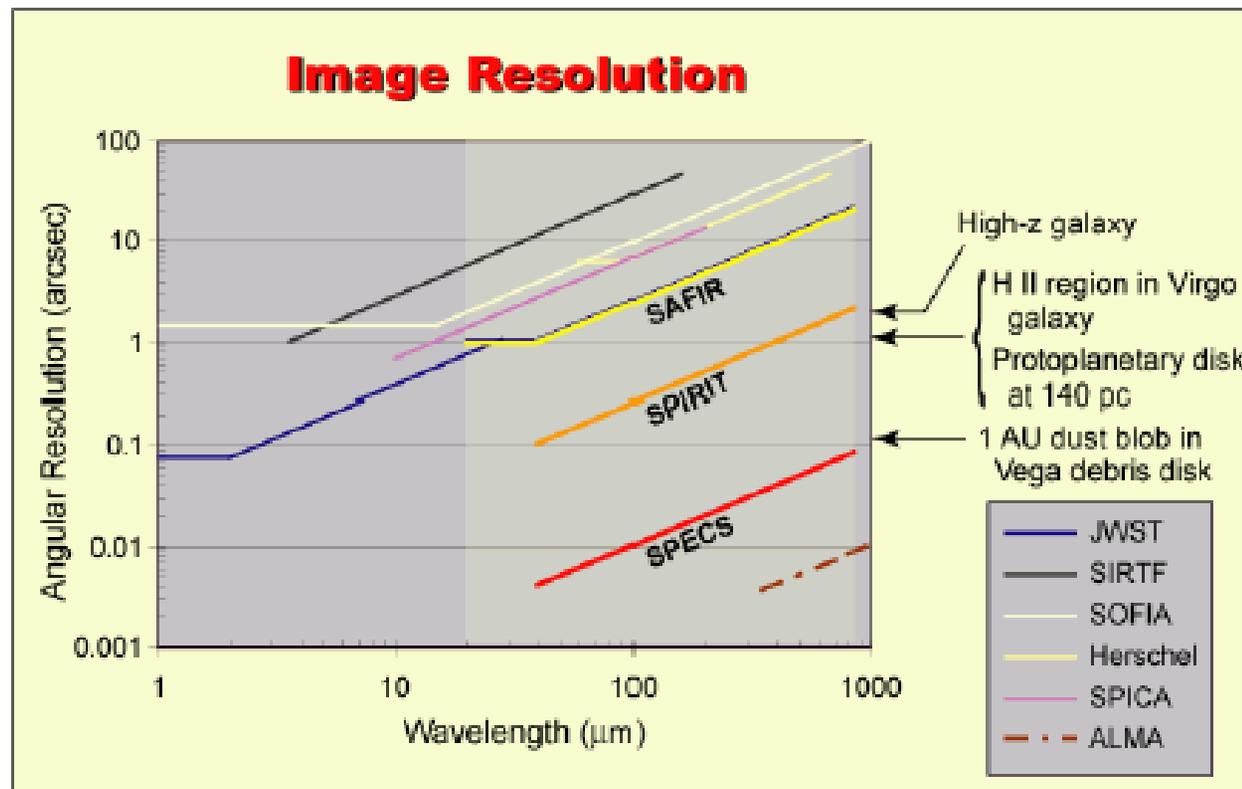
- **COTRs**
 - ⇒ Dr. H. Philip Stahl
 - ⇒ John West
- **NASA MSFC XRCF Cryogenic Test Team**
 - ⇒ Jack “Cary” Reily
 - ⇒ Jeff Kegley
 - ⇒ Harlan Haight
 - ⇒ John Tucker
 - ⇒ Ernest “Ernie” Wright
 - ⇒ William “Bill” Hogue

• **THANK YOU!!!**

- **NASA Cryogenic Mirror Needs**
- **Phase I Objectives**
- **What is SLMS™?**
- **Manufacturing Process**
- **SLMS™ Past Cryo Performance**
- **Phase I Hardware**
- **Experimental Set-Up**
- **Phase I Results**
- **Phase II Project**

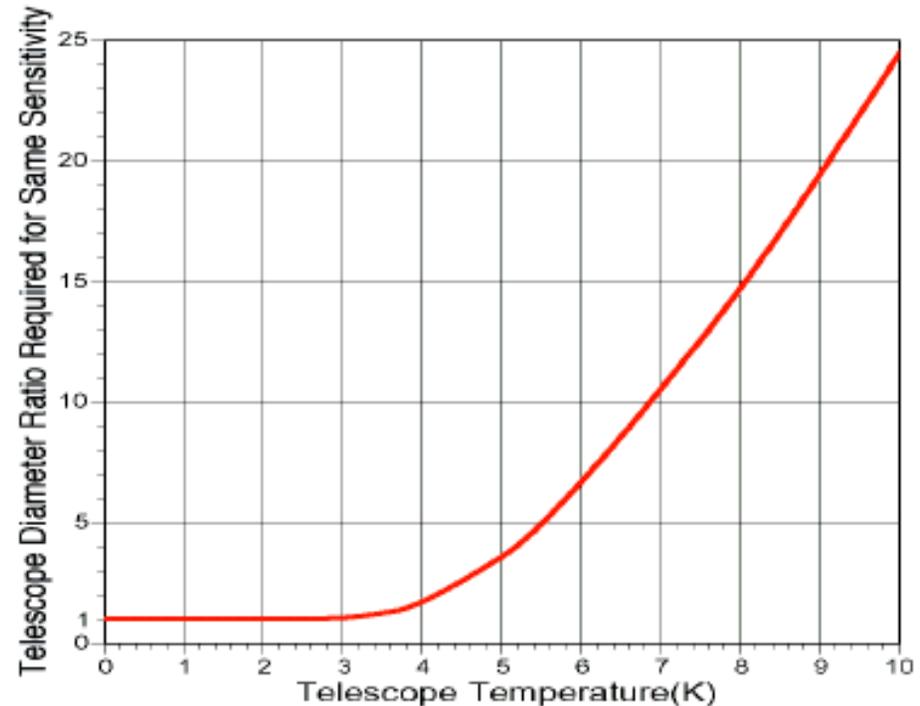
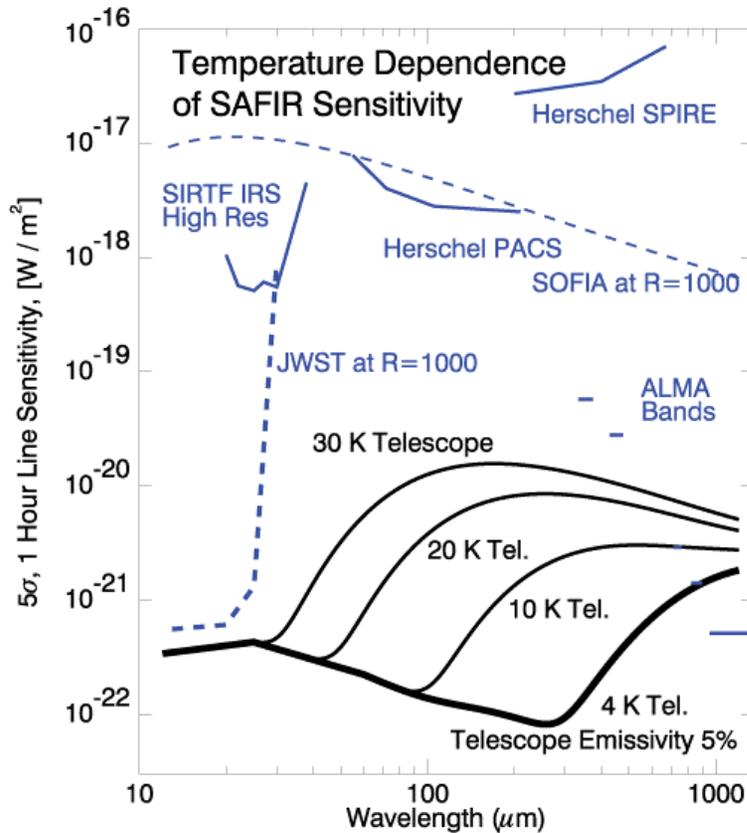
NASA Cryogenic Mirror Needs

- **Future FIR/SMM Missions (20-800 μm bandwidth) Require Optics With:**
 - ⇒ 10-25 m, areal density $<5 \text{ kg/m}^2$, surface figure specification $=\lambda/14$ at 20 μm .
- **An order of magnitude improvement in angular resolution above JWST, SIRTF, SPICA, SOPHIA and Herschel (current technologies) is required to resolve extragalactic source confusion, the individual sources of interest, and achieve the science goals of NASA's Origins and SEU themes.**



NASA Needs continued

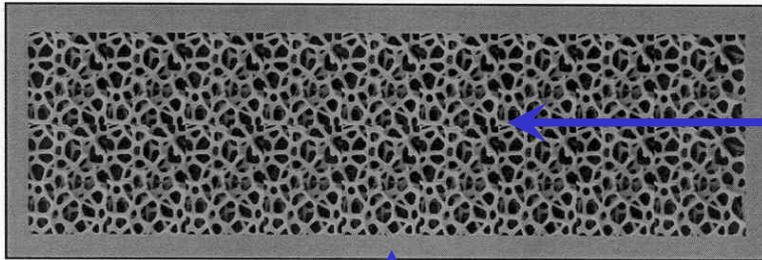
- Performance Premium for Operation at 4 Kelvin
- Point Source Sensitivity More Dependent on Temperature than Aperture at 200 μm
- 4 Kelvin Requires Active Cooling



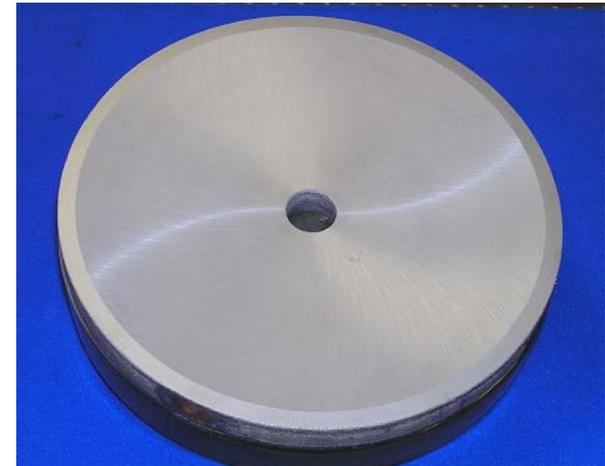
Phase I Objectives

- **Demonstrate 2 different methods for actively cooling 5-7.5 kg/m² areal density Silicon Lightweight Mirrors (SLMS™) technology for future NASA far infrared and sub-millimeter missions.**
- **Direct internal cooling will be demonstrated by directly flowing liquid nitrogen through the continuous open cell core of the SLMS™.**
- **Indirect external cooling will be demonstrated by flowing liquid nitrogen through a CTE matched C/SiC manifold that is bonded to the SLMS™.**
Simulates other types of external Cooling:
 - ⇒ **Radiative Cooling Using a Cold Plate**
 - ⇒ **Active Cooling By Conduction Using an Attached Cooler**
- **Helium Testing to 4 Kelvin to be Performed**

- **Foam Core Optics with a Continuous Shell**

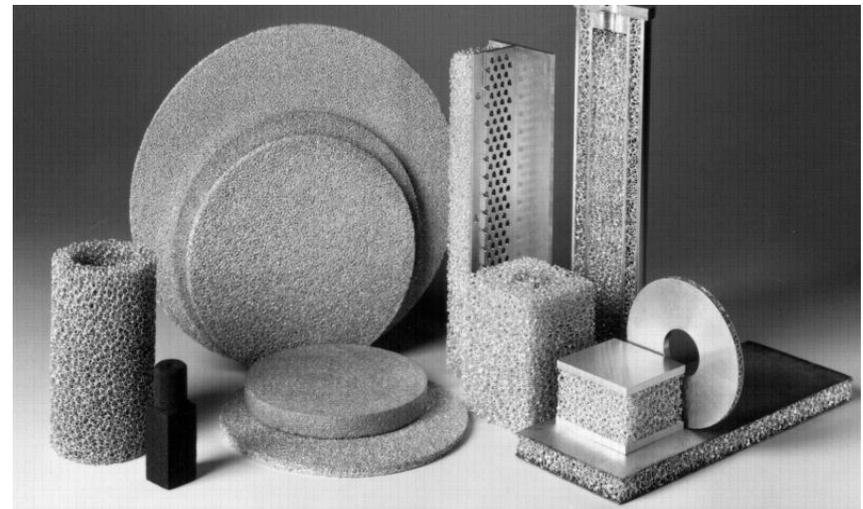


Silicon
or
Silicon Carbide
Foam



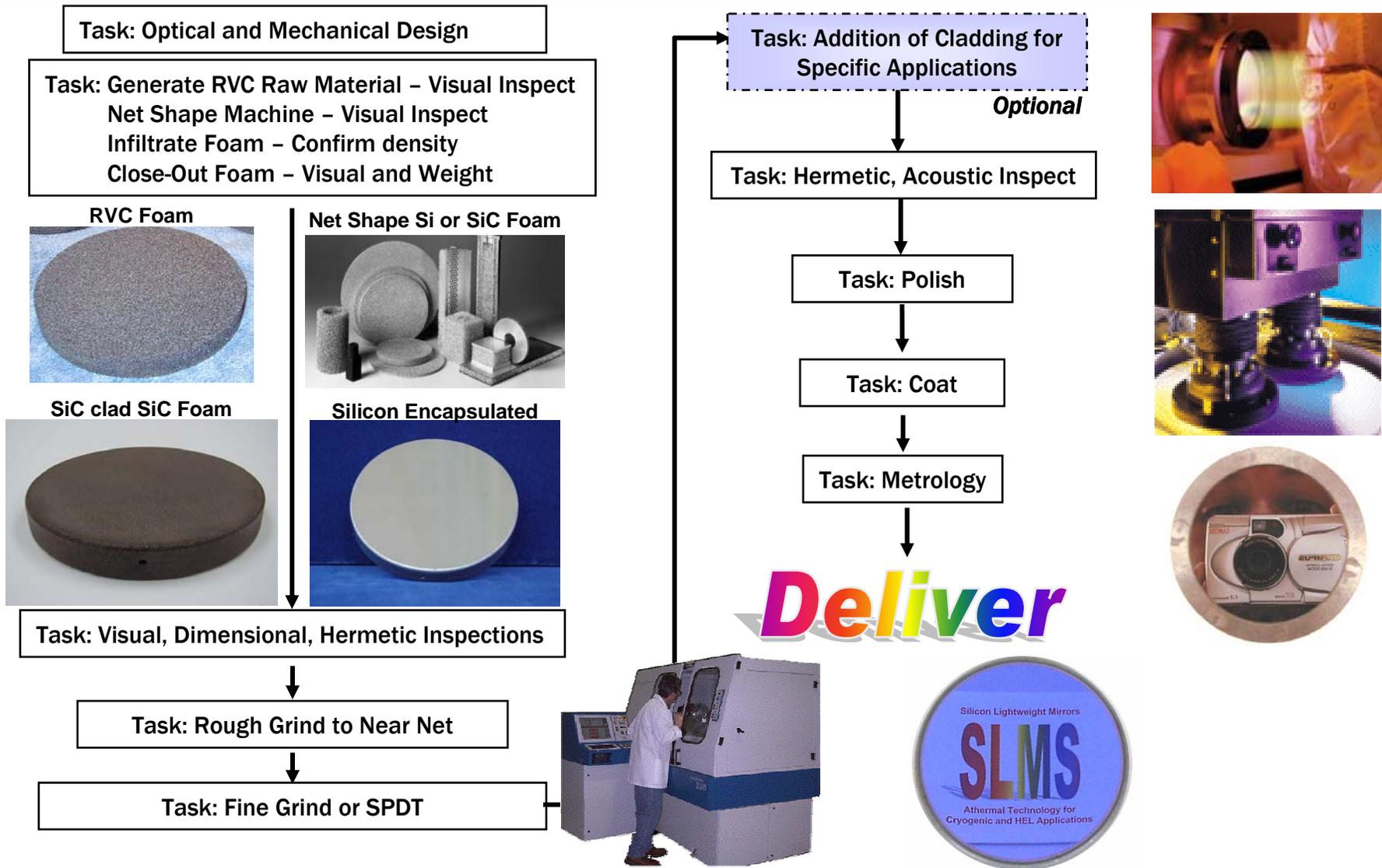
Polycrystalline Silicon or Beta-Silicon Carbide
Closeout 0.25-1.27 mm typical (0.01-0.05 inch)

- **Foam is Open-Cell, 70-95% Porosity**
- **Pore Size: 0.40 - 4.0 per mm (10-100 per inch)**
- **1500-2000 ft² surface area/ft³**
- **CNC machined to virtually any shape to $\pm 50 \mu\text{m}$ (0.002 inch)**



Design Flexibility with Large Manufacturing Basis

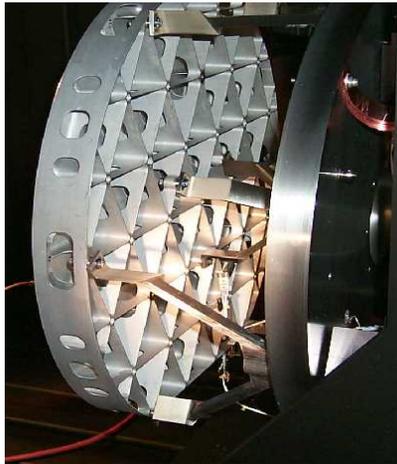
SLMS™ Manufacturing Process



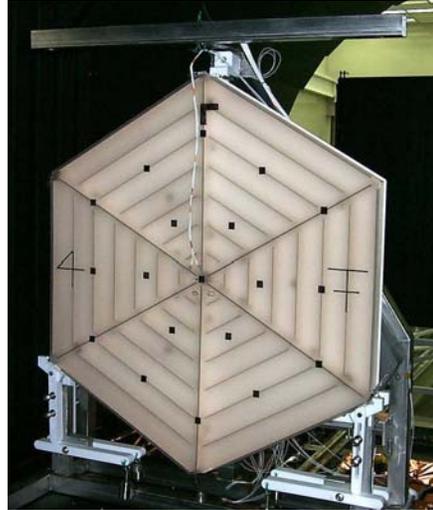
Cost Less Than Beryllium – Polishes Like Glass – ISO9001 Processes

SLMS™ Passive Cryogenic Performance

How Do SLMS™ Compare to Lightweight Be, SiC and Glass Mirrors at Cryo?



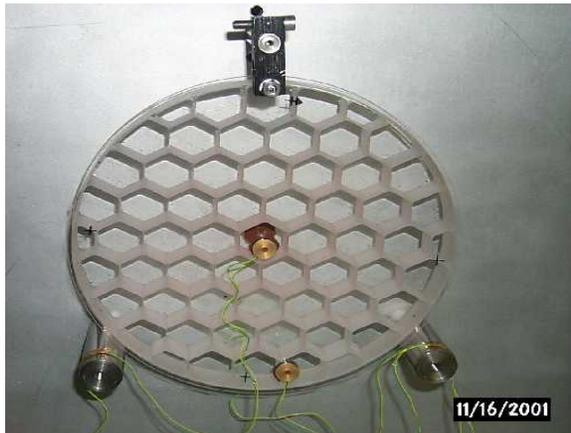
Ball Be SBMD



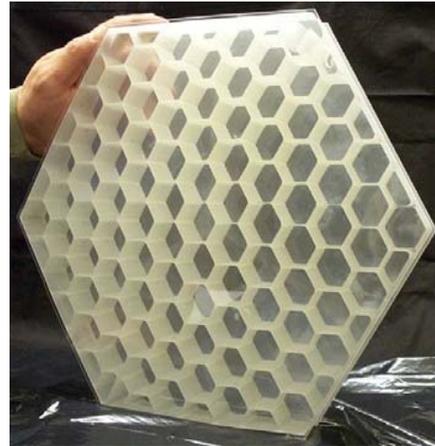
COI Zerodur/Comp NMSD



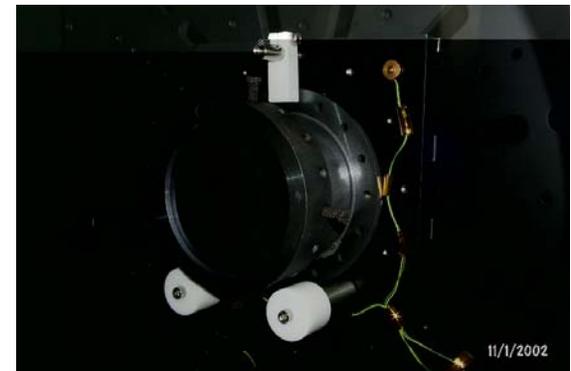
Xinetics SiC, IABG C/SiC, & Goodrich Joined-Be



Kodak Subscale SiO₂



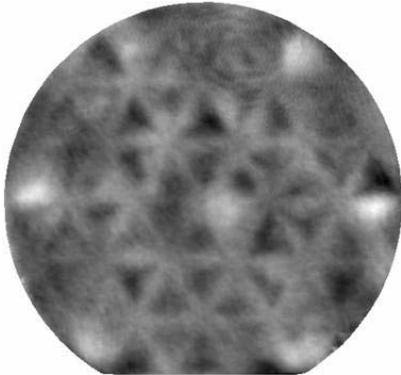
Kodak Subscale ULE



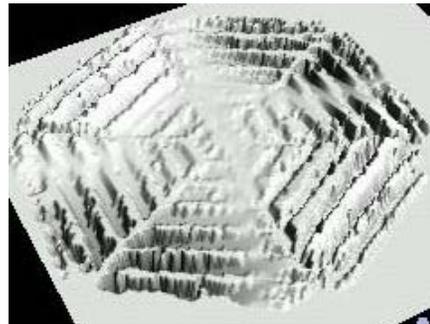
Schafer SLMS™

Data Courtesy of NASA and UAH, SPIE 2003

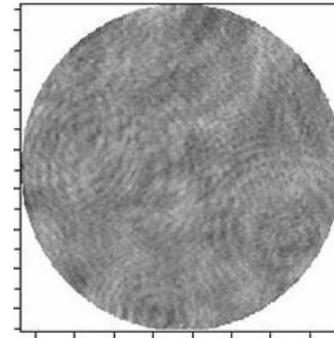
Cryogenic Performance – 27 Kelvin



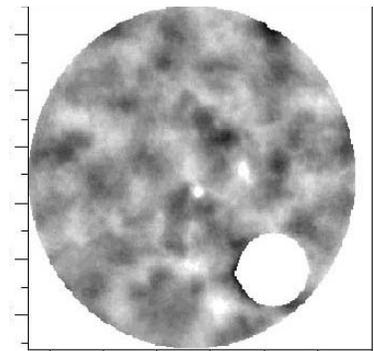
Ball Be SBMD
D=.5m, R=20m,
9.8 kg/m²
17 nm RMS



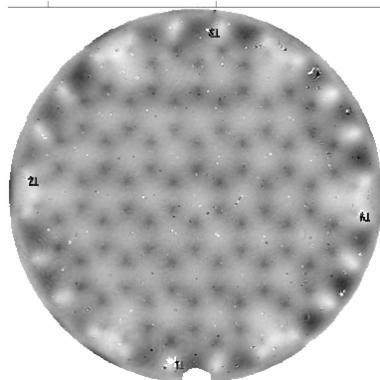
COI Zerodur/Comp NMSD
D=1.6m, R=15m,
11 kg/m²
650 nm RMS



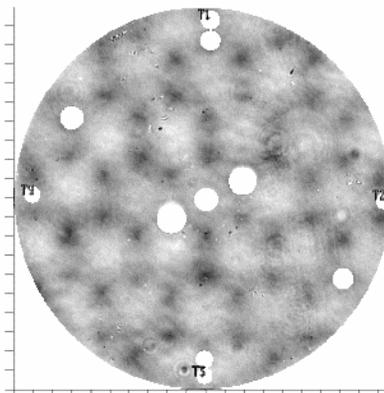
Xinetics SiC, D=.5m, R=20m
22 kg/m², 6.6 nm RMS



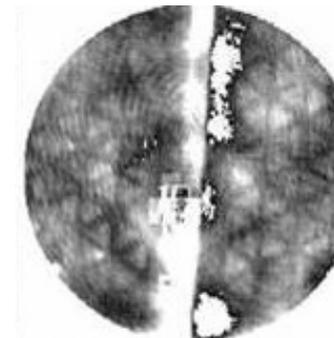
IABG C/SiC
D=.5m, R=20m,
8 kg/m²
31 nm RMS



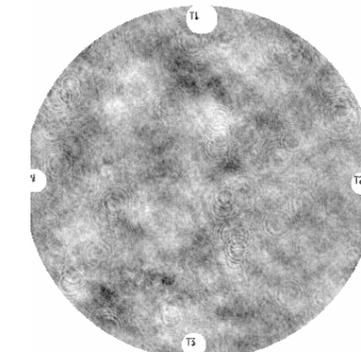
Kodak Subscale SiO₂
D=.23m, R=1.3m
10 kg/m²
17 nm RMS



Kodak Subscale ULE
D=.36m, R=1.2m
10 kg/m²
8.4 nm RMS



Goodrich Joined-Be
D=.5m, R=20m
15 nm RMS

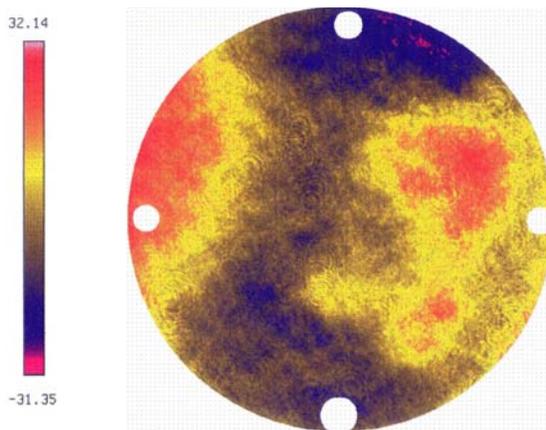


Schafer SLMS™
D=.12m, R=0.6m
9.8 kg/m²
3.7 nm RMS
Lowest Print-Through

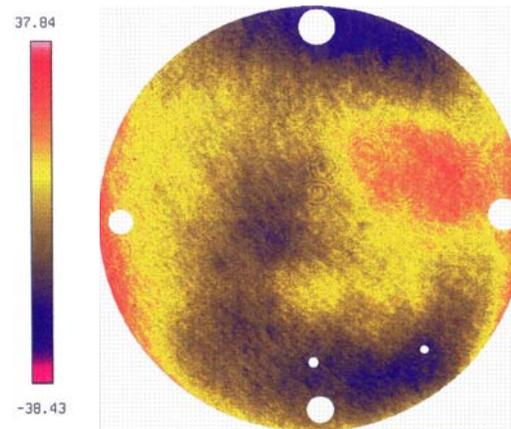
Data Courtesy of NASA and UAH, SPIE 2003

Coated vs Uncoated at Cryo

- Successfully applied HEL mirror Very Low Absorption (VLA) coatings to SLMS™
- 5-micron thick, 20-pair dielectric coating, validated at 27 K
 - ⇒ Difference of 0.5 nm rms measured after coating



Uncoated: 10.40 nm rms



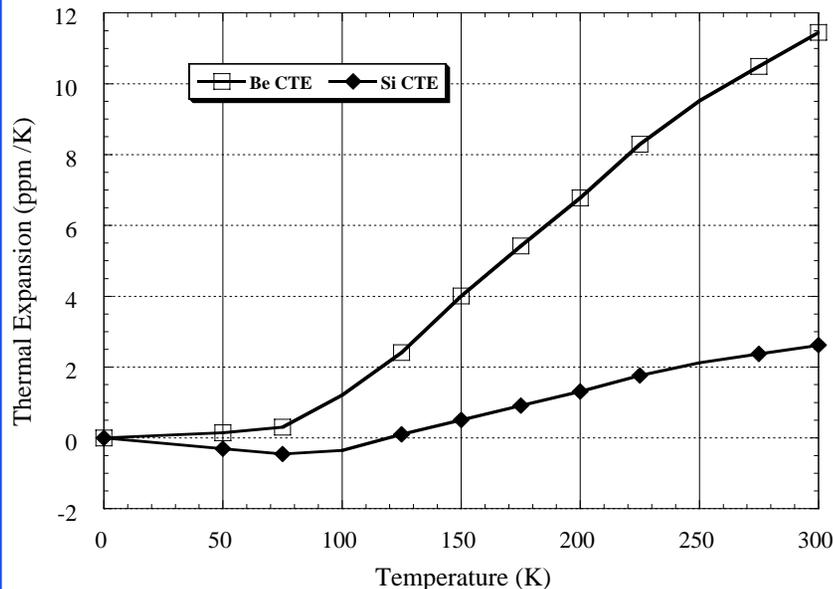
Coated: 10.92 nm rms

Coating Does Not Degrade SLMS™ Figure Performance

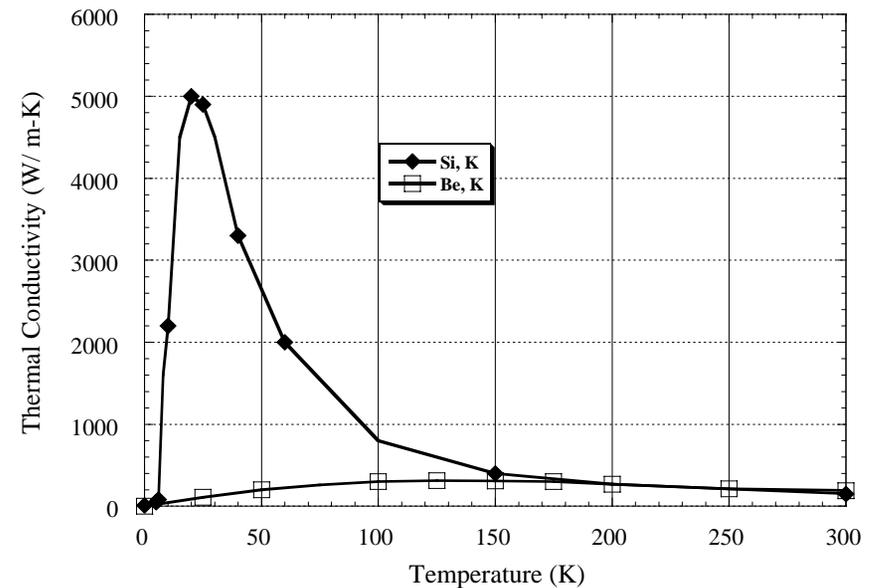
Silicon vs Beryllium – Thermal Comparison

	ρ	E	E/ρ	σ_t	σ_t/ρ	α	k	C_p	$D=k/\rho C_p$	α/k	α/D	ν
Room Temperature Property:	Density	Young's Modulus	Specific Stiffness	Tensile Strength	Specific Strength	Thermal Expansion	Thermal Conductivity	Specific Heat	Thermal Diffusivity	Steady State Distortion	Transient Distortion	Poisson's Ratio
Units:	kg/m ³	GPa	MPa·m ³ /kg	Mpa	MPa·m ³ /kg	10 ⁻⁶ /K	W/m·K	J/kg·K	10 ⁻⁶ /m ² /s	μm/W	s/m ² ·K	arbitrary
Preferred Value:	Small	Large	Large	Large	Large	Small	Large	Large	Large	Small	Small	
Beryllium:l-70	1850	287	155	237	0.13	11.3	216	1920	60.81	0.05	0.19	0.25
Silicon SLMS™ Skin	2330	130	56	120	0.05	2.5	148	750	84.69	0.02	0.03	0.24
Beta-SiC-SLMS™ Skin	3210	465	145	470	0.15	2.2	300	640	146.03	0.01	0.02	0.21

Linear Coefficient of Thermal Expansion for Silicon and Beryllium

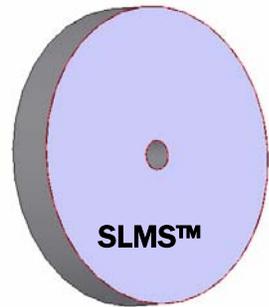


Thermal Conductivity of Silicon and Beryllium



Si has superior thermal performance than Be with similar Structural Properties

Structural Efficiency Comparison



Mirror	1st frequency (kHz)	Mass (kg)	Areal Density (kg/m ²)
ULE	1.76	0.98	16.1
Zerodur	1.93	1.12	18.4
Beryllium	3.98	0.81	13.3
SLMS, design A	3.98	0.75	12.3
SLMS, design B	4.29	0.81	13.3
SiCSLMS	5.24	0.81	13.3

- **SLMS™ same 1st Frequency as Be, at 93% the weight of Be**
- **SLMS™ same weight as Be, at 108% 1st Frequency**
- **SiC-SLMS™ same weight as Be at 131% 1st Frequency**

Stiffer than Be at Same Mass; Lighter at Same Stiffness

Phase I Hardware

SURROGATE



Invar Swagelok® butt weld VCR glands for cryo-fluid delivery and bond fixture



Cryogenic Far Infrared Submillimeter Mirror C-FISMM was Single Point Diamond Turned

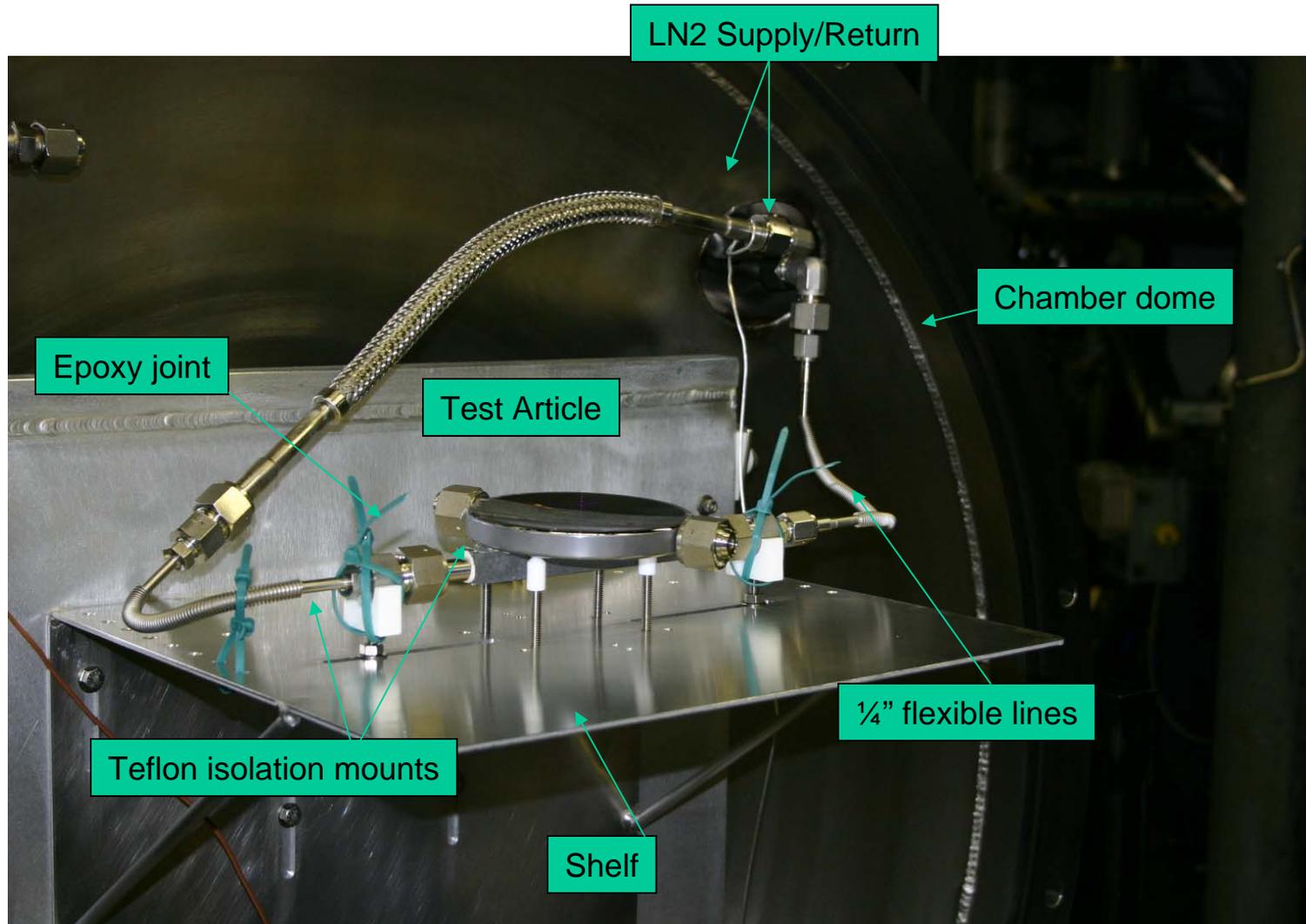


C/SiC External Manifold



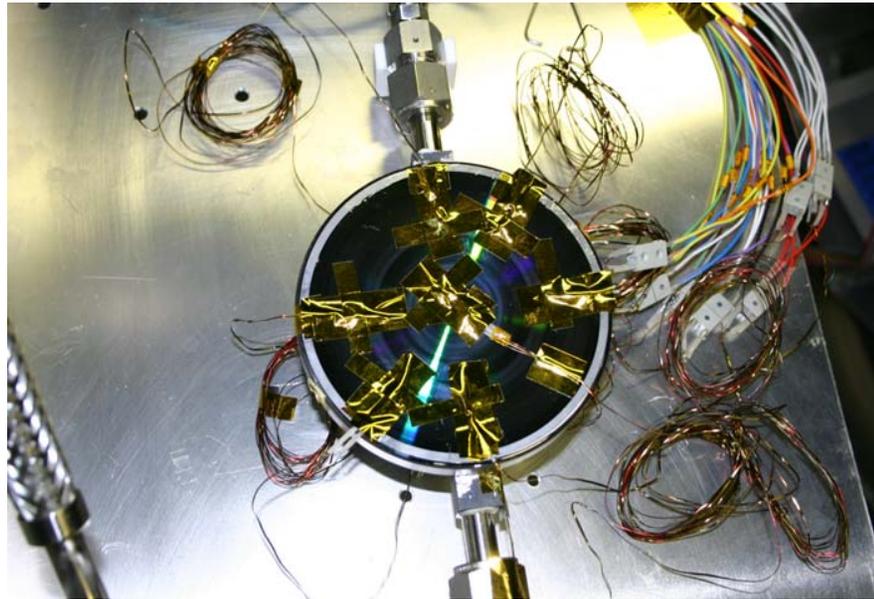
Assembly Check

Test Assembly



4-Foot Vacuum-Ambient Chamber Pumped Down to 10^{-3} Torr for Testing

Schafer Setup for External and Internal Cooling



External Flow: Mon 19 July 2004
No Insulation

← N



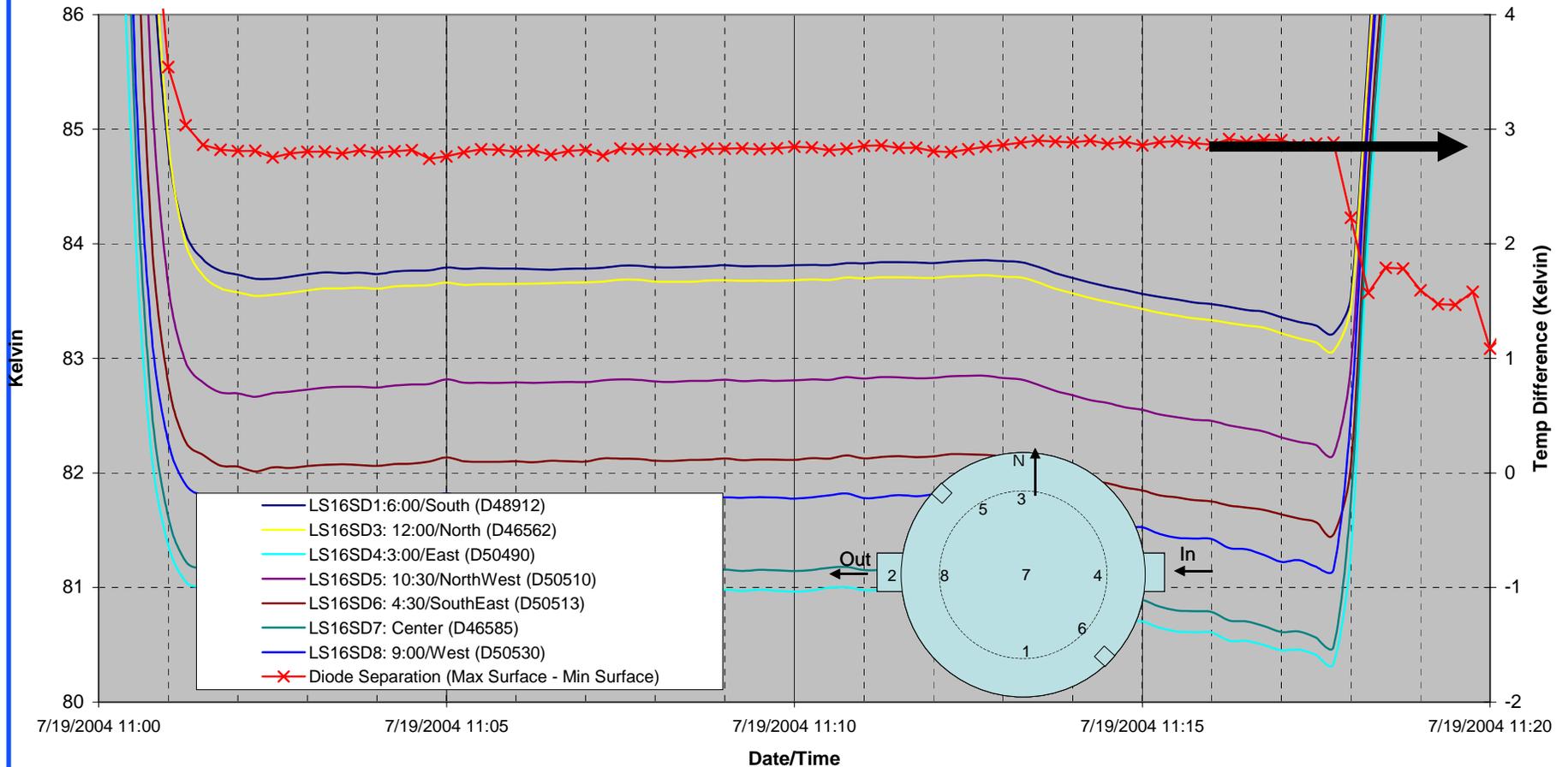
Internal Flow: Tues 20 July & Wed 21 July 2004
No Insulation

↑ N

No picture available. Diode LS16SD8 was remounted and a multi-layer insulation blanket was placed over the entire test setup.

Internal Flow with MLI Insulating Blanket: Thurs 22 July 2004

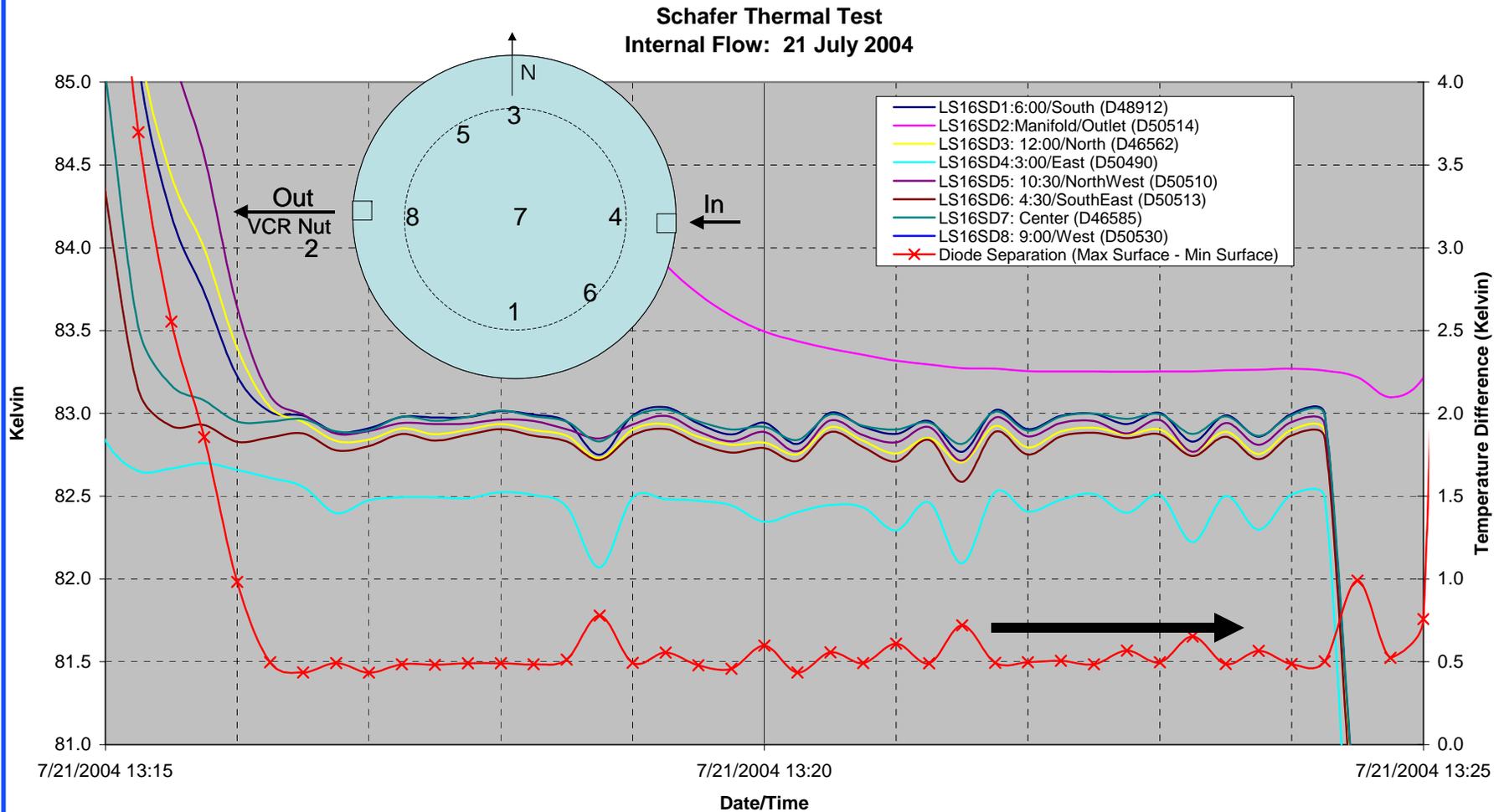
Schafer Thermal Test
External Flow: 19 July 2004



Note: The manifold diode (LS16SD2) detached during cooldown. Not included in difference calculation.

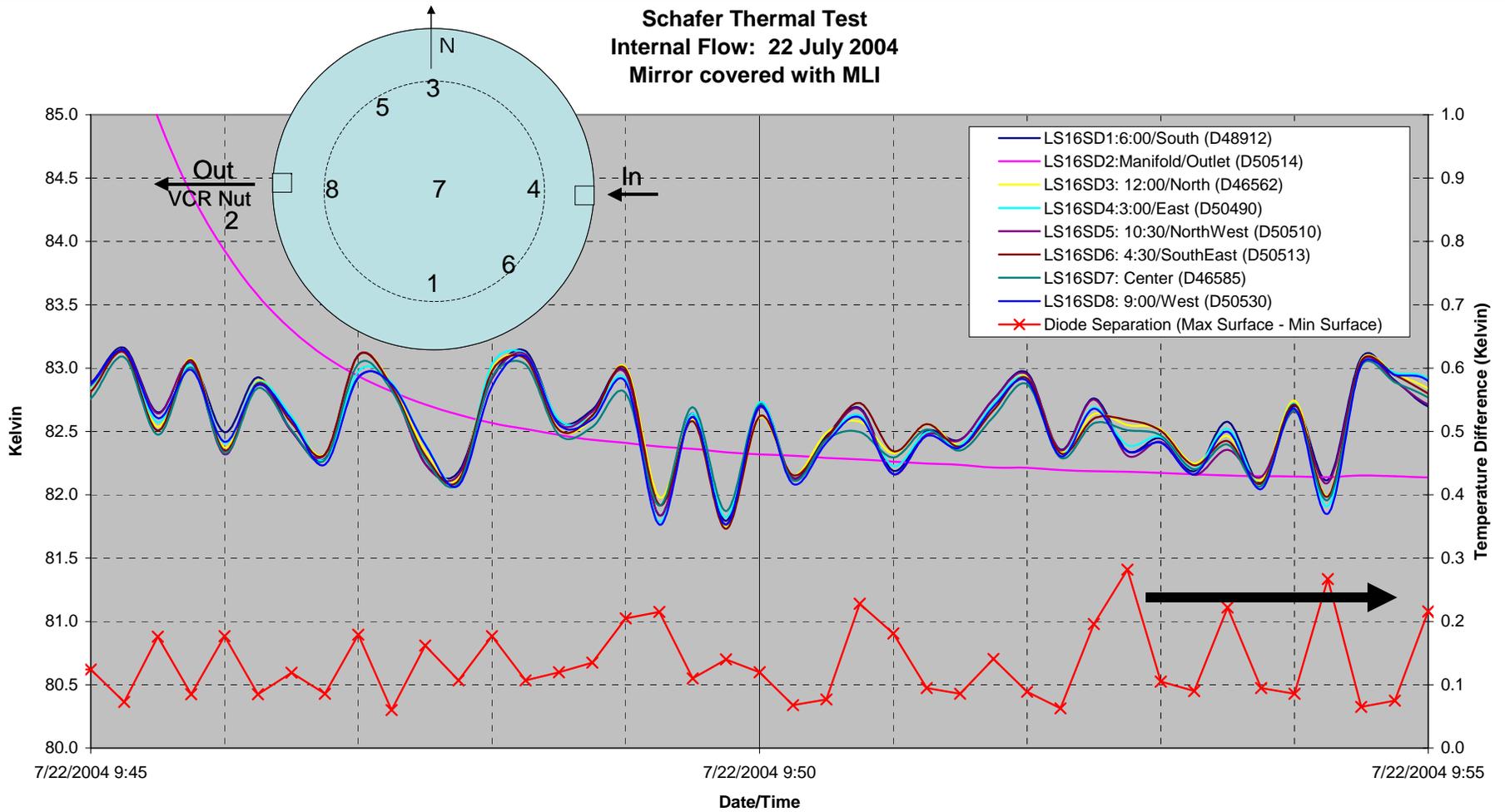
Mirror Reaches Steady State @ 82.4 ± 1.45 Kelvin in <4 minutes

Internal Flow – No Mirror Insulation



Mirror Reaches Steady State @ 82.75 ± 0.25 Kelvin in <4 minutes

Internal Flow – Insulated Mirror



Notes: LS16SD2 was mounted to the SS VCR nut; not included in difference calculation.

Mirror Reaches Steady State @ 82.75 ± 0.075 Kelvin

- Build 0.5 m Actively Cooled SLMS™ with ROC = 5 m
- Cryotest at Ball
- Cryotest at NASA MSFC in Small or Large Chamber
- Continue Technology Maturation